

# Impact Study of Limited Operation for Generator Interconnection

**GEN-2011-016**

**GEN-2011-017**

**June 2014**  
**Generator Interconnection**



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## Executive Summary

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This study report addresses the request of two separate Interconnection Customers (GEN-2011-016 and GEN-2011-017) to interconnect their requested generators before the completion of all network upgrades identified in their interconnection studies. The two Interconnection Customer's generation totals 499.1 MW of nameplate generation. The following Limited Operation System Impact Study under the Southwest Power Pool Open Access Transmission Tariff (OATT) addresses the interconnection of 499.1 MW of generation to be interconnected as an Energy Resource (ER) into the Transmission System of Sunflower Electric Power Corporation (SUNC). GEN-2011-016 is located in Ford County, Kansas. GEN-2011-017 is located in Hodgeman County, Kansas. Under the GIA Section 5.9, these Customers have requested this Limited Operation Interconnection Study (LOIS) to determine the impacts of interconnecting to the transmission system before all required Network Upgrades identified in the DISIS-2011-001 (or most recent iteration) Impact Study can be placed into service.

This LOIS addresses the effects of interconnecting the generators to the rest of the transmission system for the system topology and conditions as expected on December 31, 2015. GEN-2011-016 is requesting the interconnection of eighty seven (87) Siemens SWT 2.3 MW wind turbine generators and associated facilities into the Spearville 345kV substation. GEN-2011-017 is requesting the interconnection of one-hundred thirty (130) Siemens 2.3 MW wind turbine generators and associated facilities through a tap on Spearville – Post Rock 345kV transmission line. For the typical LOIS, both a power flow and transient stability analysis are conducted. The LOIS assumes that only the higher queued projects listed within Table 1 of this study might go into service before the completion of all Network Upgrades identified within Table 2 of this report. If additional generation projects, listed within Table 4, with queue priority equal to or higher than the study project request rights to go into commercial operation before all Network Upgrades identified within Table 2 of this report are completed, this LOIS may need to be restudied to ensure that interconnection service remains for the customer's request.

Power flow analysis from this LOIS has determined that the customer's request will be able to interconnect as an Energy Resource prior to the completion of the required Network Upgrades, listed within Table 3 of this report. Refer to Table 5 and 6 for the power flow results. Should any other projects, other than those listed within Table 1 of this report, come into service an additional study may be required to determine if any limited operation service is available. It should be noted that although this LOIS analyzed many of the most probable contingencies, it is not an all-inclusive list that can account for every operational situation. Additionally, the generator(s) may not be able to inject any power onto the Transmission System due to constraints that fall below the threshold of mitigation for a Generator Interconnection request. Because of this, it is likely that the Customers may be required to reduce their generation output to 0 MW under certain system conditions to allow system operators to maintain the reliability of the transmission network. Transient stability analysis from this LOIS has determined that the transmission system will remain stable for the one-hundred five (105) selected faults for the limited operation interconnection of GEN-2011-016 and GEN-2011-017.

Nothing in this study should be construed as a guarantee of delivery or transmission service. If the customer wishes to sell power from the facility, a separate request for transmission service must be requested on Southwest Power Pool's OASIS by the Customer.

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## Purpose

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<OMITTED TEXT> (Interconnection Customers) have requested a restudy of a Limited Operation System Impact Study (LOIS) under the Southwest Power Pool (SPP) Open Access Transmission Tariff (OATT) for interconnection requests into the Transmission System of Sunflower Electric Power Corporation (SUNC).

The purpose of this study is to evaluate the impacts of interconnecting GEN-2011-016, a request of 200.1 MW comprised of eighty seven (87) Siemens SWT 2.3 MW wind turbine generators and associated facilities interconnecting into the Spearville 345kV substation to be located in Ford County, Kansas, and GEN-2011-017, a request of 299.0 MW comprised of one-hundred thirty (130) Siemens 2.3 MW wind turbine generators and associated facilities through a tap on Spearville – Post Rock 345kV transmission line to be located in Hodgeman County, Kansas. The Customers have requested this amount to be studied as an Energy Resource (ER) with a Limited Operation Interconnection Service to commence on or around 12/31/2015.

Both power flow and transient stability analysis were conducted for this Limited Operation Interconnection Service. Limited Operation Studies are conducted under GIA Section 5.9.

The LOIS considers the Base Case as well as all Generating Facilities (and with respect to (b) below, any identified Network Upgrades associated with such higher queued interconnection) that, on the date the LOIS is commenced:

- a) are directly interconnected to the Transmission System;
- b) are interconnected to Affected Systems and may have an impact on the Interconnection Request;
- c) have a pending higher queued Interconnection Request to interconnect to the Transmission System listed in Table 1; or
- d) have no Queue Position but have executed an LGIA or requested that an unexecuted LGIA be filed with FERC.

Any changes to these assumptions, for example, one or more of the previously queued requests not included within this study execute an interconnection agreement and commencing commercial operation, may require a re-study of this LOIS at the expense of the Customer.

Nothing within this System Impact Study constitutes a request for transmission service or confers upon the Interconnection Customer any right to receive transmission service rights. Should the Customer require transmission service, those rights should be requested through SPP's Open Access Same-Time Information System (OASIS).

This LOIS study included prior queued generation interconnection requests. Those listed within Table 1 are the generation interconnection requests that are assumed to have rights to either full or partial interconnection service prior to the requested 12/31/2015 in-service of the customers for this LOIS. Also listed in Table 1 are both the amount of MWs of interconnection service expected at

the effective time of this study and the total MWs requested of interconnection service, the fuel type, the point of interconnection (POI), and the current status of each particular prior queued request.

*Table 1: Generation Requests Included within LOIS*

Project	MW	Total MW	Fuel Source	POI	Status
Gray County Wind (Montezuma)	110.0	110.0	Wind	Gray County Tap 115kV	Commercial Operation
GEN-2001-039A (Shooting Star)	105.0	105.0	Wind	Shooting Star Tap 115kV	Commercial Operation
GEN-2001-039M (Central Plains)	99.0	99.0	Wind	Central Plains Tap 115kV	Commercial Operation
GEN-2002-025A (KCPL)	148.5	148.5	Wind	Spearville 230kV	Commercial Operation
GEN-2003-006A (Meridian Way)	200.0	200.0	Wind	Elm Creek 230kV	Commercial Operation
GEN-2003-019 (Smoky Hills)	249.3	249.3	Wind	Smoky Hills Tap 230kV	Commercial Operation
GEN-2004-014 (KCPL)	154.5	154.5	Wind	Spearville 230kV	Commercial Operation
GEN-2005-012 (Westar)	248.4	248.4	Wind	Spearville 345kV	Commercial Operation
GEN-2006-006	205.5	205.5	Wind	Spearville 345kV	IA Executed/On Suspension
GEN-2006-021 (Flat Ridge I)	101.0	101.0	Wind	Flat Ridge Tap 138kV	Commercial Operation
GEN-2007-040 (Cimarron II)	200.1	200.1	Wind	Buckner 345kV	Commercial Operation
GEN-2008-018	250.0	250.0	Wind	Finney 345kV	Commercial Operation
GEN-2008-079 (Ensign)	98.9	98.9	Wind	Tap Cudahy – Ft Dodge 115kV	Commercial Operation
GEN-2008-124	200.1	200.1	Wind	Ironwood 345kV	IA Executed/On Schedule for 1/2016
GEN-2010-009 (Cimarron I)	165.6	165.6	Wind	Buckner 345kV	Commercial Operation
GEN-2010-045	197.8	197.8	Wind	Buckner 345kV	IA Executed/On Schedule for 2017
GEN-2010-057	201.0	201.0	Wind	Rice County 230kV	Commercial Operation
GEN-2011-008	600.0	600.0	Wind	Clark County 345kV	IA Executed/ On Schedule for 2019
GEN-2011-014	201.0	201.0	Wind	Beaver County 345kV	IA Pending
GEN-2011-019	299.0	299.0	Wind	Woodward 345kV	IA Executed/On Schedule for 2017
GEN-2011-020	299.0	299.0	Wind	Woodward 345kV	IA Executed/On Schedule for 2017
GEN-2011-016	200.1	200.1	Wind	Spearville 345kV	IA Pending
GEN-2011-017	299.0	299.0	Wind	Tap Spearville – Post Rock 345kV	IA Executed/On Schedule for 2017

This LOIS was required because the Customers are requesting interconnection prior to the completion of all of their required upgrades listed within the latest iteration of their Definitive Interconnection System Impact Study (DISIS). Table 2 below lists the required upgrade projects for which these requests have cost responsibility. Table 3 below lists the projects that are not in-service at the time of the Customers in-service date and are not included in this LOIS study. The customers were included within the DISIS-2011-001 that was posted July 29, 2011. The cluster has been restudied since the original posting. This report can be located here at the following GI Study URL:

[http://sppoasis.spp.org/documents/swpp/transmission/GenStudies.cfm?YearType=2011\\_Impact\\_Studies](http://sppoasis.spp.org/documents/swpp/transmission/GenStudies.cfm?YearType=2011_Impact_Studies).

*Table 2: Upgrade Projects Required for Full Interconnection Service*

<b>Upgrade Project</b>	<b>Type</b>	<b>Description</b>	<b>Status</b>
Beaver County – Buckner 345kV	Assumed out of service for the study	Contingent on DISIS-2011-001 Customers	Current Estimated In-Service date unknown
Spearville – Post Rock – Axtell 345kV	Assumed to be in service for the study	Build Priority Project	In Service
Woodward – Border – TUCO 345kV and associated equipment	Assumed to be in service for the study	Build Priority Project	Current Estimated In-Service date of 5/19/2014
Hitchland – Woodward 345kV double circuit and associated equipment	Assumed to be in service for the study	Build Priority Project	Current Estimated in service date of 6/30/2014
Spearville – Clark County – Thistle – Wichita 345kV double circuit and associated equipment	Assumed to be in service for the study	Build Priority Project	Current Estimated In-Service date of 12/31/2014
Woodward – Thistle 345kV double circuit and associated equipment	Assumed to be in service for the study	Build Priority Project	Current Estimated In-Service date of 12/31/2014

*Table 3: Upgrade Projects Not Included in this Study*

<b>Upgrade Project</b>	<b>Type</b>	<b>Description</b>	<b>Status</b>
Beaver County – Buckner 345kV	Assumed out of service for the study	Contingent on DISIS-2011-001 Customers	Current Estimated In-Service date unknown

Any changes to these assumptions, for example, one or more of the previously queued requests not included within this study execute an interconnection agreement and commencing commercial operation, may require a re-study of this LOIS at the expense of the Customer. The higher or equally queued projects that were not included in this study are listed in Table 4. While this list is not all inclusive it is a list of the most probable and affecting prior queued requests that were not included within this LOIS, either because no request for an LOIS has been made or the request is on suspension, etc.

*Table 4: Higher or Equally Queued GI Requests not included within this LOIS*

<b>Project</b>	<b>Remainder MW</b>	<b>Total MW</b>	<b>Fuel</b>	<b>POI</b>	<b>Status</b>
GEN-2007-038	200.0	200.0	Wind	Spearville 345kV	IA Executed/On Schedule for 8/2015
GEN-2010-015	200.1	200.1	Wind	Spearville 345kV	IA Executed/On Schedule for 1/2015

Nothing in this System Impact Study constitutes a request for transmission service or grants the Interconnection Customer any rights to transmission service.



# Facilities

## Generating Facility

GEN-2011-016 Interconnection Customer’s request to interconnect a total of 200.1 MW is comprised of eighty seven (87) Siemens SWT 2.3 MW wind turbine generators and associated facilities. GEN-2011-017 Interconnection Customer’s request to interconnect a total of 299.0 MW is comprised of one-hundred thirty (130) Siemens 2.3 MW wind turbine generators and associated facilities.

## Interconnection Facilities

### GEN-2011-016

The POI for GEN-2011-016 Interconnection Customer is the Spearville 345kV substation in Ford County, Kansas. Figure 1 depicts the one-line diagram of the local transmission system including the POI as well as the power flow model representing the request.

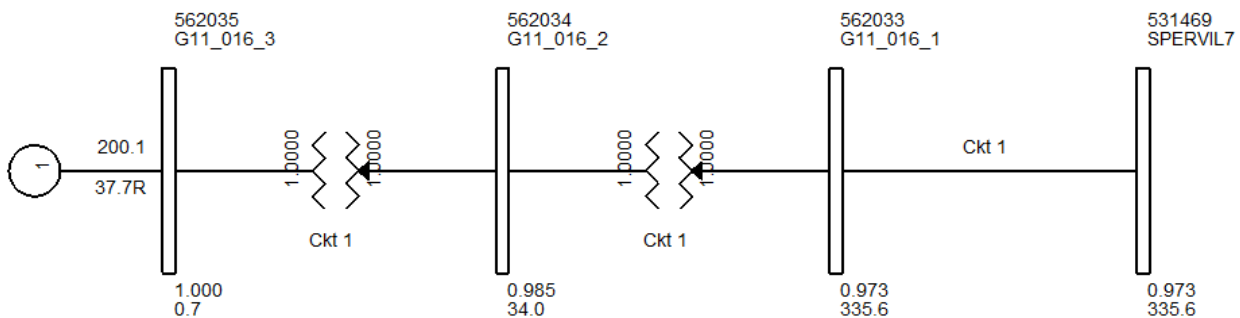


Figure 1: Proposed POI Configuration and Request Power Flow Model

### GEN-2011-017

The POI for GEN-2011-017 Interconnection Customer is through a tap on the Spearville – Post Rock 345kV transmission line in Hodgeman County, Kansas. Figure 2 depicts the one-line diagram of the local transmission system including the POI as well as the power flow model representing the request.

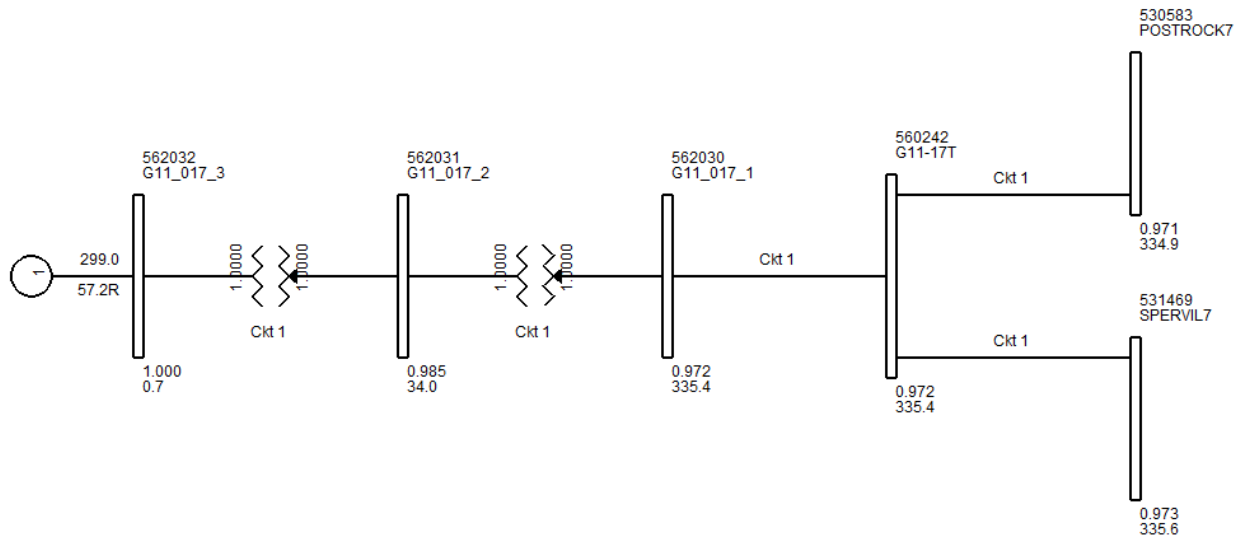


Figure 2: Proposed POI Configuration and Request Power Flow Model

### Base Case Network Upgrades

The Network Upgrades included within the cases used for this LOIS study are those facilities that are a part of the SPP Transmission Expansion Plan or the Balanced Portfolio projects that have in-service dates prior to the Customers requested in-service date of December 31, 2015. These facilities have an approved Notification to Construct (NTC), or are in construction stages and expected to be in-service at the effective time of this study. No other upgrades were included for this LOIS. If for some reason, construction on these projects is delayed or discontinued, a restudy may be needed to determine the interconnection service availability of the Customer(s).

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# Power Flow Analysis

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Power flow analysis is used to determine if the transmission system can accommodate the injection from the request without violating thermal or voltage transmission planning criteria.

## Model Preparation

Power flow analysis was performed using modified versions of the 2013 series of transmission service request study models including the 2014 and 2019 (spring, summer, and winter) seasonal models. To incorporate the Interconnection Customer's request, a re-dispatch of existing generation within SPP was performed with respect to the amount of the Customer's injection and the interconnecting Balancing Authority. This method allows the request to be studied as an Energy Resource (ERIS) Interconnection Request. For this LOIS, only the previous queued requests listed in Table 1 were assumed to be in-service.

## Study Methodology and Criteria

The ACCC function of PSS/E is used to simulate contingencies, including single and multiple facility (i.e. breaker-to-breaker, etc.) outages, within all of the control areas of SPP and other control areas external to SPP and the resulting data analyzed. This satisfies the "more probable" contingency testing criteria mandated by NERC and the SPP criteria.

The contingency set includes all SPP control area branches and ties 69kV and above, first tier Non-SPP control area branches and ties 115 kV and above, any defined contingencies for these control areas, and generation unit outages for the SPP control areas with SPP reserve share program redispatch.

The monitor elements include all SPP control area branches, ties, and buses 69 kV and above, and all first tier Non-SPP control area branches and ties 69 kV and above. NERC Power Transfer Distribution Flowgates for SPP and first tier Non-SPP control area are monitored. Additional NERC Flowgates are monitored in second tier or greater Non-SPP control areas. Voltage monitoring was performed for SPP control area buses 69 kV and above.

## Results

The LOIS ACCC analysis indicates that the Customers can interconnect their generation into the SUNC transmission system as requested before all required upgrades listed within the DISIS-2011-001 study can be placed into service. Should any other GI projects, other than those listed within Table 1 of this report, come into service an additional study may be required to determine if any limited operation service is available.

ACCC results for the LOIS can be found in Table 5, 6 and 7 below. Table 7 has the overloads that are less than 20% TDF and are not for mitigation. Generator Interconnection Energy Resource analysis doesn't mitigate for those issues in which the affecting GI request has less than a 20% OTDF.

## **Curtailment and System Reliability**

In no way does this study guarantee operation for all periods of time. It should be noted that although this study analyzed many of the most probable contingencies, it is not an all-inclusive list and cannot account for every operational situation. Because of this, it is likely that the Customer may be required to reduce their generation output to 0 MW under certain system conditions to allow system operators to maintain the reliability of the transmission network.

Power Flow Analysis

Table 5: Interconnection Constraints for Reinforcement of GEN-2011-016 LOIS @ 200.1MW

Season	Dispatch Group	Flow	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Max MW Available	Contingency
ALL			N/A					200.1	N/A

Table 6: Interconnection Constraints for Reinforcement of GEN-2011-017 LOIS @ 299.0MW

Season	Dispatch Group	Flow	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Max MW Available	Contingency
ALL			N/A					299.0	N/A

Table 7: Interconnection Constraints that do not require reinforcement

Season	Dispatch Group	Flow	Source	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Contingency
14G	03ALL	-	G11_016	Non-converged Contingency	-	-	0.44933	-	DBL-THIS-CLR
14G	03ALL	-	G11_017	Non-converged Contingency	-	-	0.41101	-	DBL-THIS-CLR
14G	03ALL	-	G11_016	Non-converged Contingency	-	-	0.44933	-	DBL-IRON-CLR
14G	03ALL	-	G11_017	Non-converged Contingency	-	-	0.41101	-	DBL-IRON-CLR
14G	03G11_016	-	G11_016	Non-converged Contingency	-	-	0.45043	-	DBL-THIS-CLR
14G	03G11_017	-	G11_017	Non-converged Contingency	-	-	0.41213	-	DBL-THIS-CLR
14G	3	-	G11_016	Non-converged Contingency	-	-	0.45047	-	DBL-THIS-CLR
14G	3	-	G11_017	Non-converged Contingency	-	-	0.41215	-	DBL-THIS-CLR
14G	03ALL	FROM->TO	G11_016	HARPER - MILAN TAP 138KV CKT 1	110	110	0.05349	242.3275	DBL-WICH-THI
14G	03ALL	FROM->TO	G11_017	HARPER - MILAN TAP 138KV CKT 1	110	110	0.04821	242.3275	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_016	CLEARWATER - MILAN TAP 138KV CKT 1	110	110	0.05349	231.9561	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_017	CLEARWATER - MILAN TAP 138KV CKT 1	110	110	0.04821	231.9561	DBL-WICH-THI
14G	03G11_016	FROM->TO	G11_016	HARPER - MILAN TAP 138KV CKT 1	110	110	0.05379	207.1276	DBL-WICH-THI
14G	03G11_017	FROM->TO	G11_017	HARPER - MILAN TAP 138KV CKT 1	110	110	0.04851	205.8021	DBL-WICH-THI
14G	3	FROM->TO	G11_016	HARPER - MILAN TAP 138KV CKT 1	110	110	0.05381	202.7553	DBL-WICH-THI
14G	3	FROM->TO	G11_017	HARPER - MILAN TAP 138KV CKT 1	110	110	0.04852	202.7553	DBL-WICH-THI
14G	03G11_016	TO->FROM	G11_016	CLEARWATER - MILAN TAP 138KV CKT 1	110	110	0.05379	196.6507	DBL-WICH-THI
14G	03G11_017	TO->FROM	G11_017	CLEARWATER - MILAN TAP 138KV CKT 1	110	110	0.04851	195.3139	DBL-WICH-THI
14G	3	TO->FROM	G11_016	CLEARWATER - MILAN TAP 138KV CKT 1	110	110	0.05381	192.2473	DBL-WICH-THI
14G	3	TO->FROM	G11_017	CLEARWATER - MILAN TAP 138KV CKT 1	110	110	0.04852	192.2473	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.05374	159.2001	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04956	159.2001	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04473	143.1289	NORTHWEST - TATONGA7 345.00 345KV CKT 1

Power Flow Analysis

Season	Dispatch Group	Flow	Source	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Contingency
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04214	143.1289	NORTHWEST - TATONGA7 345.00 345KV CKT 1
14G	03G11_016	TO->FROM	G11_016	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.049	138.2562	DBL-IRON-CLR
14G	03ALL	TO->FROM	G11_016	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04872	137.6726	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_017	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04415	137.6726	DBL-SPRVL-CL
14G	03G11_017	TO->FROM	G11_017	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04443	137.0446	DBL-IRON-CLR
14G	3	TO->FROM	G11_016	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04901	134.4715	DBL-IRON-CLR
14G	3	TO->FROM	G11_017	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04444	134.4715	DBL-IRON-CLR
14G	03G11_016	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.054	130.9307	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04473	130.1034	TATONGA7 345.00 - WOODWARD DISTRICT EHV 345KV CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04214	130.1034	TATONGA7 345.00 - WOODWARD DISTRICT EHV 345KV CKT 1
14G	03G11_017	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04983	130.0066	DBL-WICH-THI
14G	3	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.05401	127.6158	DBL-WICH-THI
14G	3	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04984	127.6158	DBL-WICH-THI
14G	03G11_016	FROM->TO	G11_016	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.049	127.3446	DBL-IRON-CLR
14G	03ALL	FROM->TO	G11_016	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04872	126.7428	DBL-SPRVL-CL
14G	03ALL	FROM->TO	G11_017	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04415	126.7428	DBL-SPRVL-CL
14G	03ALL	FROM->TO	G11_016	CLEARWATER - GILL ENERGY CENTER WEST 138KV CKT 1	191	191	0.05349	126.4919	DBL-WICH-THI
14G	03ALL	FROM->TO	G11_017	CLEARWATER - GILL ENERGY CENTER WEST 138KV CKT 1	191	191	0.04821	126.4919	DBL-WICH-THI
14G	03G11_017	FROM->TO	G11_017	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04443	126.1517	DBL-IRON-CLR
14G	03ALL	TO->FROM	G11_016	HAYS PLANT - SOUTH HAYS 115KV CKT 1	83	99	0.03348	125.596	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03ALL	TO->FROM	G11_017	HAYS PLANT - SOUTH HAYS 115KV CKT 1	83	99	0.04423	125.596	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03ALL	TO->FROM	G11_016	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.09442	125.5295	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_017	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.0946	125.5295	DBL-WICH-THI
14G	3	FROM->TO	G11_016	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04901	123.5959	DBL-IRON-CLR
14G	3	FROM->TO	G11_017	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04444	123.5959	DBL-IRON-CLR
14G	03G11_016	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04495	123.446	NORTHWEST - TATONGA7 345.00 345KV CKT 1
14G	03G11_017	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04236	122.7301	NORTHWEST - TATONGA7 345.00 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.13615	122.39	G11-17T 345.00 - POST ROCK 345KV CKT 1
14G	03ALL	TO->FROM	G11_017	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.13615	122.39	G11-17T 345.00 - POST ROCK 345KV CKT 1
14G	03G11_016	TO->FROM	G11_016	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.049	122.3869	DBL-IRON-CLR
14G	03ALL	TO->FROM	G11_016	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.04872	121.6688	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_017	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.04415	121.6688	DBL-SPRVL-CL
14G	03G11_017	TO->FROM	G11_017	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.04443	121.1911	DBL-IRON-CLR
14G	3	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04496	120.867	NORTHWEST - TATONGA7 345.00 345KV CKT 1
14G	3	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04237	120.867	NORTHWEST - TATONGA7 345.00 345KV CKT 1
14G	3	TO->FROM	G11_016	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.04901	118.6288	DBL-IRON-CLR
14G	3	TO->FROM	G11_017	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.04444	118.6288	DBL-IRON-CLR

Power Flow Analysis

Season	Dispatch Group	Flow	Source	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Contingency
14G	03ALL	FROM->TO	G11_016	HAYS PLANT - VINE STREET 115KV CKT 1	80	88	0.03348	118.2057	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03ALL	FROM->TO	G11_017	HAYS PLANT - VINE STREET 115KV CKT 1	80	88	0.04423	118.2057	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03ALL	FROM->TO	G11_016	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.08033	116.9323	DBL-WICH-THI
14G	03ALL	FROM->TO	G11_017	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.09474	116.9323	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03521	116.6253	WOODWARD (WOODWRD2) 138/69/13.2KV TRANSFORMER CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03321	116.6253	WOODWARD (WOODWRD2) 138/69/13.2KV TRANSFORMER CKT 1
14G	03G11_016	TO->FROM	G11_016	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.049	115.8444	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03134	115.6664	GEN520997 1-MORLND2
14G	03G11_017	TO->FROM	G11_017	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04443	114.6522	DBL-SPRVL-CL
14G	03G11_016	TO->FROM	G11_016	HAYS PLANT - SOUTH HAYS 115KV CKT 1	83	99	0.03356	113.6311	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03G11_017	TO->FROM	G11_017	HAYS PLANT - SOUTH HAYS 115KV CKT 1	83	99	0.04431	113.4488	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03689	112.8634	IODINE - WOODWARD EHV 138KV CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03481	112.8634	IODINE - WOODWARD EHV 138KV CKT 1
14G	3	TO->FROM	G11_016	HAYS PLANT - SOUTH HAYS 115KV CKT 1	83	99	0.03355	112.5403	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	3	TO->FROM	G11_017	HAYS PLANT - SOUTH HAYS 115KV CKT 1	83	99	0.0443	112.5403	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	3	TO->FROM	G11_016	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04901	112.0108	DBL-SPRVL-CL
14G	3	TO->FROM	G11_017	GREENSBURG - SSTARTP3 115.00 115KV CKT 1	115.1	115.1	0.04444	112.0108	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03689	111.0928	DEWEY - IODINE 138KV CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03481	111.0928	DEWEY - IODINE 138KV CKT 1
14G	03G11_016	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04495	110.7676	TATONGA7 345.00 - WOODWARD DISTRICT EHV 345KV CKT 1
14G	03G11_017	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04236	110.0534	TATONGA7 345.00 - WOODWARD DISTRICT EHV 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03134	109.3366	GEN520998 1-MORLND3
14G	3	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04496	108.2042	TATONGA7 345.00 - WOODWARD DISTRICT EHV 345KV CKT 1
14G	3	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.04237	108.2042	TATONGA7 345.00 - WOODWARD DISTRICT EHV 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.10944	107.6955	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_017	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.08246	107.6955	DBL-WICH-THI
14G	03G11_016	FROM->TO	G11_016	SEWARD - ST JOHN 115KV CKT 1	80.3	87.6	0.03733	106.834	DBL-IRON-CLR
14G	03G11_016	FROM->TO	G11_016	CLEARWATER - GILL ENERGY CENTER WEST 138KV CKT 1	191	191	0.05379	106.2679	DBL-WICH-THI
14G	03G11_017	FROM->TO	G11_017	SEWARD - ST JOHN 115KV CKT 1	80.3	87.6	0.03777	106.0142	DBL-IRON-CLR
14G	03G11_017	FROM->TO	G11_017	CLEARWATER - GILL ENERGY CENTER WEST 138KV CKT 1	191	191	0.04851	105.505	DBL-WICH-THI
14G	03G11_016	FROM->TO	G11_016	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.049	105.1089	DBL-SPRVL-CL
14G	03G11_016	TO->FROM	G11_016	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.09491	104.9406	DBL-WICH-THI
14G	03ALL	FROM->TO	G11_016	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.07805	104.8508	AXTELL - POST ROCK 345KV CKT 1
14G	03ALL	FROM->TO	G11_017	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.10102	104.8508	AXTELL - POST ROCK 345KV CKT 1

Power Flow Analysis

Season	Dispatch Group	Flow	Source	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Contingency
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03664	104.7913	THISTLE7 345.00 - WICHITA 345KV CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03431	104.7913	THISTLE7 345.00 - WICHITA 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03664	104.7913	THISTLE7 345.00 - WICHITA 345KV CKT 2
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03431	104.7913	THISTLE7 345.00 - WICHITA 345KV CKT 2
14G	03ALL	TO->FROM	G11_016	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.07863	104.7636	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1
14G	03ALL	TO->FROM	G11_017	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.08573	104.7636	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1
14G	03ALL	TO->FROM	G11_016	KNOLL - N HAYS3 115.00 115KV CKT 1	80	88	0.03348	104.7327	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03ALL	TO->FROM	G11_017	KNOLL - N HAYS3 115.00 115KV CKT 1	80	88	0.04423	104.7327	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03G11_016	FROM->TO	G11_016	HAYS PLANT - VINE STREET 115KV CKT 1	80	88	0.03356	104.6776	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03G11_017	FROM->TO	G11_017	HAYS PLANT - VINE STREET 115KV CKT 1	80	88	0.04431	104.4762	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	03G11_016	TO->FROM	G11_016	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.13015	104.4351	DBL-IRON-CLR
14G	03G11_017	TO->FROM	G11_017	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.09509	104.2587	DBL-WICH-THI
14G	03G11_017	FROM->TO	G11_017	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04443	103.9231	DBL-SPRVL-CL
14G	3	FROM->TO	G11_016	CLEARWATER - GILL ENERGY CENTER WEST 138KV CKT 1	191	191	0.05381	103.7559	DBL-WICH-THI
14G	3	FROM->TO	G11_017	CLEARWATER - GILL ENERGY CENTER WEST 138KV CKT 1	191	191	0.04852	103.7559	DBL-WICH-THI
14G	3	FROM->TO	G11_016	HAYS PLANT - VINE STREET 115KV CKT 1	80	88	0.03355	103.4823	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	3	FROM->TO	G11_017	HAYS PLANT - VINE STREET 115KV CKT 1	80	88	0.0443	103.4823	KNOLL 230 - POSTROCK6 230.00 230KV CKT 1
14G	3	FROM->TO	G11_016	SEWARD - ST JOHN 115KV CKT 1	80.3	87.6	0.03734	103.4133	DBL-IRON-CLR
14G	3	FROM->TO	G11_017	SEWARD - ST JOHN 115KV CKT 1	80.3	87.6	0.03778	103.4133	DBL-IRON-CLR
14G	03G11_016	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03149	103.1973	GEN520997 1-MORLND2
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03138	103.1926	LAWTON EASTSIDE - OKLAUNION 345KV CKT 1
14G	03ALL	FROM->TO	G11_016	CUDAHY - KISMET 3 115.00 115KV CKT 1	115.1	115.1	0.03129	103.1689	BUCKNER7 345.00 - HOLCOMB 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03755	103.0171	RENFROW7 345.00 - VIOLA 7 345.00 345KV CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03577	103.0171	RENFROW7 345.00 - VIOLA 7 345.00 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03521	102.9374	WOODWARD - WOODWARD 69KV CKT 1
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03321	102.9374	WOODWARD - WOODWARD 69KV CKT 1
14G	03G11_017	TO->FROM	G11_017	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.12797	102.9354	DBL-IRON-CLR
14G	03ALL	TO->FROM	G11_016	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.12967	102.4658	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_017	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.12748	102.4658	DBL-SPRVL-CL
14G	3	TO->FROM	G11_016	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.09494	102.1993	DBL-WICH-THI
14G	3	TO->FROM	G11_017	CIRCLE - MULLERGREN 230KV CKT 1	318.7	318.7	0.09511	102.1993	DBL-WICH-THI
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03134	102.0201	BASE CASE
14G	03G11_016	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03537	101.6442	WOODWARD (WOODWRD2) 138/69/13.2KV TRANSFORMER CKT 1
14G	03ALL	TO->FROM	G11_016	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.13615	101.6296	G11-17T 345.00 - SPEARVILLE 345KV CKT 1
14G	3	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03149	101.579	GEN520997 1-MORLND2
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03219	101.3967	RENFROW7 345.00 (BANK 1) 345/138/13.8KV TRANSFORMER CKT 1



Power Flow Analysis

Season	Dispatch Group	Flow	Source	Overloaded Element	RATEA (MVA)	RATEB (MVA)	TDF	TC% LOADING	Contingency
14G	03ALL	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03052	101.3967	RENFROW7 345.00 (BANK 1) 345/138/13.8KV TRANSFORMER CKT 1
14G	3	FROM->TO	G11_016	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04901	101.3023	DBL-SPRVL-CL
14G	3	FROM->TO	G11_017	GREENSBURG - SUN CITY 115KV CKT 1	115.1	115.1	0.04444	101.3023	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_016	CIMARRON RIVER TAP - KISMET 3 115.00 115KV CKT 1	115.1	115.1	0.03129	101.2887	BUCKNER7 345.00 - HOLCOMB 345KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03157	101.1081	SPP-SWPS-03
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03156	101.1058	ELK CITY 230KV (ELKCTY-6) 230/138/13.8KV TRANSFORMER CKT 1
14G	03G11_017	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03337	101.1025	WOODWARD (WOODWRD2) 138/69/13.2KV TRANSFORMER CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03156	101.0937	ELK CITY 230KV - SWEETWATER 230KV CKT 1
14G	03G11_016	TO->FROM	G11_016	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.13663	101.0936	G11-17T 345.00 - POST ROCK 345KV CKT 1
14G	03G11_016	FROM->TO	G11_016	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.11237	100.7785	DBL-IRON-CLR
14G	03G11_017	TO->FROM	G11_017	MULLERGREN - SPEARVILLE 230KV CKT 1	398	398	0.13663	100.3235	G11-17T 345.00 - POST ROCK 345KV CKT 1
14G	03ALL	FROM->TO	G11_016	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.07055	100.2846	CIRCLE - MULLERGREN 230KV CKT 1
14G	03ALL	FROM->TO	G11_017	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.08806	100.2846	CIRCLE - MULLERGREN 230KV CKT 1
14G	03G11_017	FROM->TO	G11_017	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.12459	100.2507	DBL-IRON-CLR
14G	03G11_016	TO->FROM	G11_016	MEDICINE LODGE - SUN CITY 115KV CKT 1	115.1	115.1	0.049	100.1286	DBL-SPRVL-CL
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.0314	100	RENFROW4 138.00 - SAND RDG_138138.00 138KV CKT 1
14G	03ALL	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03156	100	GRAPEVINE INTERCHANGE - STATELINE INTERCHANGE 230KV CKT 1
14G	3	TO->FROM	G11_016	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03537	99.7	WOODWARD (WOODWRD2) 138/69/13.2KV TRANSFORMER CKT 1
14G	3	TO->FROM	G11_017	FPL SWITCH - WOODWARD 138KV CKT 1	133	153	0.03338	99.7	WOODWARD (WOODWRD2) 138/69/13.2KV TRANSFORMER CKT 1
14G	03ALL	FROM->TO	G11_016	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.11198	99.6	DBL-SPRVL-CL
14G	03ALL	FROM->TO	G11_017	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.1242	99.6	DBL-SPRVL-CL
14G	03G11_016	FROM->TO	G11_016	SMOKYHL6 230.00 - SUMMIT 230KV CKT 1	330	330	0.08071	99.6	DBL-WICH-THI

## Stability Analysis

Transient stability analysis is used to determine if the transmission system can maintain angular stability and ensure bus voltages stay within planning criteria bandwidth during and after a disturbance while considering the addition of a generator interconnection request.

### Model Preparation

Transient stability analysis was performed using modified versions of the 2013 series of Model Development Working Group (MDWG) dynamic study models including the 2014 winter, 2015 summer, and 2024 summer seasonal models. The cases are then adapted to resemble the power flow study cases with regards to prior queued generation requests and topology. Finally the prior queued and study generation dispatched into the SPP footprint. Initial simulations are then carried out for a no-disturbance run of twenty (20) seconds to verify the numerical stability of the model.

### Disturbances

One-hundred five (105) contingencies were identified for the Limited Operation scenario for use in this study. These faults are listed within Table 8. These contingencies included three-phase faults and single-phase line faults at locations defined by SPP. Single-phase line faults were simulated by applying fault impedance to the positive sequence network at the fault location to represent the effect of the negative and zero sequence networks on the positive sequence network. The fault impedance was computed to give a positive sequence voltage at the specified fault location of approximately 60% of pre-fault voltage. This method is in agreement with SPP current practice.

With exception to transformers, the typical sequence of events for a three-phase and single-phase fault is as follows:

1. apply fault at particular location
2. continue fault for five (5) cycles, clear the fault by tripping the faulted facility
3. after an additional twenty (20) cycles, re-close the previous facility back into the fault
4. continue fault for five (5) additional cycles
5. trip the faulted facility and remove the fault

Transformer faults are typically only performed for three-phase faults, unless otherwise noted. Additionally the sequence of events for a transformer is to 1) apply a three-phase fault for five (5) cycles and 2) clear the fault by tripping the affected transformer facility. Unless otherwise noted there will be no re-closing into a transformer fault.

*Table 8: Contingencies Evaluated for Limited Operation*

Contingency Number and Name		Description
1	FLT_001_SPERVIL7_BUCKNER7_345kV_3PH	3-Phase fault on the Buckner – Spearville 345kV CKT near the Spearville 345kV bus.
2	FLT_002_SPERVIL7_BUCKNER7_345kV_1PH	Single-phase fault similar to previous fault.
3	FLT_003_SPERVIL7_CLARKCOUNTY7_345kV_3PH	3-Phase fault on the Clark County – Spearville 345kV CKT near the Spearville 345kV bus.
4	FLT_004_SPERVIL7_CLARKCOUNTY7_345kV_1PH	Single-phase fault similar to previous fault.

Contingency Number and Name		Description
5	FLT_005_SPERVIL7_IRONWOOD7_345kV_3PH	3-Phase fault on the Ironwood – Spearville 345kV CKT near the Spearville 345kV bus.
6	FLT_006_SPERVIL7_IRONWOOD7_345kV_1PH	Single-phase fault similar to previous fault.
7	FLT_007_SPERVIL7_G11017TAP_345kV_3PH	3-Phase fault on the GEN-2011-017-Tap – Spearville 345kV CKT near the Spearville 345kV bus.
8	FLT_008_SPERVIL7_G11017TAP_345kV_1PH	Single-phase fault similar to previous fault.
9	FLT_009_SPERVIL7_SPEARVL6_345_230kV_3PH	3-Phase fault on the Spearville 345/230/13.8kV transformer near the Spearville 345kV bus.
10	FLT_010_SPERVIL7_LANCER3_345_115kV_3PH	3-Phase fault on the Spearville 345/115/13.8kV (Lancer) transformer near the Spearville 345kV bus.
11	FLT_011_BUCKNER7_HOLCOMB7_345kV_3PH	3-Phase fault on the Buckner – Holcomb 345kV CKT near the Buckner 345kV bus.
12	FLT_012_BUCKNER7_HOLCOMB7_345kV_1PH	Single-phase fault similar to previous fault.
13	FLT_013_HOLCOMB7_FINNEY7_345kV_3PH	3-Phase fault on the Finney – Holcomb 345kV CKT near the Holcomb 345kV bus.
14	FLT_014_HOLCOMB7_FINNEY7_345kV_1PH	Single-phase fault similar to previous fault.
15	FLT_015_HOLCOMB7_SETAB7_345kV_3PH	3-Phase fault on the Holcomb – Setab 345kV CKT near the Holcomb 345kV bus.
16	FLT_016_HOLCOMB7_SETAB7_345kV_1PH	Single-phase fault similar to previous fault.
17	FLT_017_HOLCOMB7_HOLCOMB3_345_115kV_3PH	3-Phase fault on the Holcomb 345/115/13.8kV transformer near the Holcomb 345kV bus.
18	FLT_018_FINNEY7_HITCHLAND7_345kV_3PH	3-Phase fault on the Finney – Hitchland 345kV CKT near the Finney 345kV bus.
19	FLT_019_FINNEY7_HITCHLAND7_345kV_1PH	Single-phase fault similar to previous fault.
20	FLT_020_IRONWOOD7_SPERVIL7_345kV_3PH	3-Phase fault on the Ironwood – Spearville 345kV CKT near the Ironwood 345kV bus.
21	FLT_021_IRONWOOD7_SPERVIL7_345kV_1PH	Single-phase fault similar to previous fault.
22	FLT_022_IRONWOOD7_CLARKCOUNTY7_345kV_3PH	3-Phase fault on the Clark County – Ironwood 345kV CKT near the Ironwood 345kV bus.
23	FLT_023_IRONWOOD7_CLARKCOUNTY7_345kV_1PH	Single-phase fault similar to previous fault.
24	FLT_024_CLARKCOUNTY7_THISTLE7_345kV_3PH	3-Phase fault on the Clark County – Thistle 345kV CKT near the Clark County 345kV bus.
25	FLT_025_CLARKCOUNTY7_THISTLE7_345kV_1PH	Single-phase fault similar to previous fault.
26	FLT_026_THISTLE7_WICHITA7_345kV_3PH	3-Phase fault on the Thistle – Wichita 345kV CKT near the Thistle 345kV bus.
27	FLT_027_THISTLE7_WICHITA7_345kV_1PH	Single-phase fault similar to previous fault.
28	FLT_028_THISTLE7_WWRDEHV7_345kV_3PH	3-Phase fault on the Thistle – Woodward 345kV CKT near the Thistle 345kV bus.
29	FLT_029_THISTLE7_WWRDEHV7_345kV_1PH	Single-phase fault similar to previous fault.
30	FLT_030_THISTLE7_THISTLE4_345_138kV_3PH	3-Phase fault on the Thistle 345/138/13.8kV transformer near the Thistle 345kV bus.
31	FLT_031_WWRDEHV7_TATONGA7_345kV_3PH	3-Phase fault on the Tatonga – Woodward 345kV CKT near the Woodward 345kV bus.
32	FLT_032_WWRDEHV7_TATONGA7_345kV_1PH	Single-phase fault similar to previous fault.
33	FLT_033_WWRDEHV7_BORDER7_345kV_3PH	3-Phase fault on the Border – Woodward 345kV CKT near the Woodward 345kV bus.
34	FLT_034_WWRDEHV7_BORDER7_345kV_1PH	Single-phase fault similar to previous fault.
35	FLT_035_WWRDEHV7_BEAVERCO_345kV_3PH	3-Phase fault on the Beaver County – Woodward 345kV CKT near the Woodward 345kV bus.
36	FLT_036_WWRDEHV7_BEAVERCO_345kV_1PH	Single-phase fault similar to previous fault.
37	FLT_037_WWRDEHV7_WWRDEHV4_345_138kV_3PH	3-Phase fault on the Woodward 345/138/13.8kV transformer near the Woodward 345kV bus.
38	FLT_038_BEAVERCO_HITCHLAND7_345kV_3PH	3-Phase fault on the Beaver County – Hitchland 345kV CKT near the Beaver County 345kV bus.
39	FLT_039_BEAVERCO_HITCHLAND7_345kV_1PH	Single-phase fault similar to previous fault.
40	FLT_040_WICHITA7_EMPEC7_345kV_3PH	3-Phase fault on the Emporia Energy Center – Wichita 345kV CKT near the Wichita 345kV bus.
41	FLT_041_WICHITA7_EMPEC7_345kV_1PH	Single-phase fault similar to previous fault.

Contingency Number and Name		Description
42	FLT_042_WICHITA7_RENO7_345kV_3PH	3-Phase fault on the Reno – Wichita 345kV CKT near the Wichita 345kV bus.
43	FLT_043_WICHITA7_RENO7_345kV_1PH	Single-phase fault similar to previous fault.
44	FLT_044_WICHITA7_BENTON7_345kV_3PH	3-Phase fault on the Benton – Wichita 345kV CKT near the Wichita 345kV bus.
45	FLT_045_WICHITA7_BENTON7_345kV_1PH	Single-phase fault similar to previous fault.
46	FLT_046_WICHITA7_VIOLA7_345kV_3PH	3-Phase fault on the Viola – Wichita 345kV CKT near the Wichita 345kV bus.
47	FLT_047_WICHITA7_VIOLA7_345kV_1PH	Single-phase fault similar to previous fault.
48	FLT_048_G11017TAP_SPERVIL7_345kV_3PH	3-Phase fault on the GEN-2011-017-Tap – Spearville 345kV CKT near the GEN-2011-017-Tap 345kV bus.
49	FLT_049_G11017TAP_SPERVIL7_345kV_1PH	Single-phase fault similar to previous fault.
50	FLT_050_G11017TAP_POSTROCK7_345kV_3PH	3-Phase fault on the GEN-2011-017-Tap – Post Rock 345kV CKT near the GEN-2011-017-Tap 345kV bus.
51	FLT_051_G11017TAP_POSTROCK7_345kV_1PH	Single-phase fault similar to previous fault.
52	FLT_052_POSTROCK7_AXTELL3_345kV_3PH	3-Phase fault on the Axtell – Post Rock 345kV CKT near the Post Rock 345kV bus.
53	FLT_053_POSTROCK7_AXTELL3_345kV_1PH	Single-phase fault similar to previous fault.
54	FLT_054_POSTROCK7_POSTROCK6_345_230kV_3PH	3-Phase fault on the Post Rock 345/230/13.8kV transformer near the Post Rock 345kV bus.
55	FLT_055_AXTELL3_PAULINE3_345kV_3PH	3-Phase fault on the Axtell – Pauline 345kV CKT near the Axtell 345kV bus.
56	FLT_056_AXTELL3_PAULINE3_345kV_1PH	Single-phase fault similar to previous fault.
57	FLT_057_AXTELL3_SWEETW3_345kV_3PH	3-Phase fault on the Axtell – Sweetwater 345kV CKT near the Axtell 345kV bus.
58	FLT_058_AXTELL3_SWEETW3_345kV_1PH	Single-phase fault similar to previous fault.
59	FLT_059_AXTELL3_AXTELL7_345_115kV_3PH	3-Phase fault on the Axtell 345/115/13.8kV transformer near the Axtell 345kV bus.
60	FLT_060_SPEARVL6_GRTBEND6_230kV_3PH	3-Phase fault on the Great Bend – Spearville 230kV CKT near the Spearville 230kV bus.
61	FLT_061_SPEARVL6_GRTBEND6_230kV_1PH	Single-phase fault similar to previous fault.
62	FLT_062_SPEARVL6_SPEARVL3_230_115kV_3PH	3-Phase fault on the Spearville 230/115/13.8kV transformer near the Spearville 230kV bus.
63	FLT_063_GRTBEND6_CIRCLE6_230kV_3PH	3-Phase fault on the Circle – Great Bend 230kV CKT near the Great Bend 230kV bus.
64	FLT_064_GRTBEND6_CIRCLE6_230kV_1PH	Single-phase fault similar to previous fault.
65	FLT_065_GRTBEND6_HEIZER6_230kV_3PH	3-Phase fault on the Great Bend – Heizer 230kV CKT near the Great Bend 230kV bus.
66	FLT_066_GRTBEND6_HEIZER6_230kV_1PH	Single-phase fault similar to previous fault.
67	FLT_067_SHAYS6_GRTBEND6_230kV_3PH	3-Phase fault on the Great Bend – South Hays 230kV CKT near the South Hays 230kV bus.
68	FLT_068_SHAYS6_GRTBEND6_230kV_1PH	Single-phase fault similar to previous fault.
69	FLT_069_POSTROCK6_SHAYS6_230kV_3PH	3-Phase fault on the Post Rock – South Hays 230kV CKT near the Post Rock 230kV bus.
70	FLT_070_POSTROCK6_SHAYS6_230kV_1PH	Single-phase fault similar to previous fault.
71	FLT_071_POSTROCK6_KNOLL6_230kV_3PH	3-Phase fault on the Knoll – Post Rock 230kV CKT near the Post Rock 230kV bus.
72	FLT_072_POSTROCK6_KNOLL6_230kV_1PH	Single-phase fault similar to previous fault.
73	FLT_073_KNOLL6_SMOKYHL6_230kV_3PH	3-Phase fault on the Knoll – Smoky Hills 230kV CKT near the Knoll 230kV bus.
74	FLT_074_KNOLL6_SMOKYHL6_230kV_1PH	Single-phase fault similar to previous fault.
75	FLT_075_SMOKYHL6_SUMMIT6_230kV_3PH	3-Phase fault on the Smoky Hills – Summit 230kV CKT near the Smoky Hills 230kV bus.
76	FLT_076_SMOKYHL6_SUMMIT6_230kV_1PH	Single-phase fault similar to previous fault.
77	FLT_077_NFTDODG3_FTDODGE3_115kV_3PH	3-Phase fault on the Fort Dodge– North Fort Dodge 115kV CKT near the North Fort Dodge 115kV bus.
78	FLT_078_NFTDODG3_FTDODGE3_115kV_1PH	Single-phase fault similar to previous fault.

Contingency Number and Name		Description
79	FLT_079_NFTDODG3_SSTATTP3_115kV_3PH	3-Phase fault on the North Fort Dodge– Shooting Star Tap 115kV CKT near the North Fort Dodge 115kV bus.
80	FLT_080_NFTDODG3_SSTATTP3_115kV_1PH	Single-phase fault similar to previous fault.
81	FLT_081_FTDODGE3_CRKCK3_115kV_3PH	3-Phase fault on the Crooked Creek Tap –Fort Dodge 115kV CKT near the Fort Dodge 115kV bus.
82	FLT_082_FTDODGE3_CRKCK3_115kV_1PH	Single-phase fault similar to previous fault.
83	FLT_083_P4SPERBUCKSPER_SPEARVL6_345_230kV_1PH	Loss of Buckner – Spearville 345kV CKT and Spearville 345/230/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Spearville 345kV bus.
84	FLT_084_P4SPERCLARSPER_SPEARVL6_345_230kV_1PH	Loss of Clark County – Spearville 345kV CKT and Spearville 345/230/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Spearville 345kV bus.
85	FLT_085_P4SPERIRONSPER_SPEARVL6_345_230kV_1PH	Loss of Ironwood – Spearville 345kV CKT and Spearville 345/230/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Spearville 345kV bus.
86	FLT_086_P4SPER1117SPER_SPEARVL6_345_230kV_1PH	Loss of GEN-2011-017-Tap – Spearville 345kV CKT and Spearville 345/230/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Spearville 345kV bus.
87	FLT_087_P4AXTEPAULAXTE_AXTELL7_345_115kV_1PH	Loss of Axtell – Pauline 345kV CKT and Axtell 345/115/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Axtell 345kV bus.
88	FLT_088_P4AXTESWEEAXTE_AXTELL7_345_115kV_1PH	Loss of Axtell – Sweetwater 345kV CKT and Axtell 345/115/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Axtell 345kV bus.
89	FLT_089_P4THISWWRDTHIS_THISTLE4_345_138kV_1PH	Loss of Thistle – Woodward 345kV CKT and Thistle 345/138/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Thistle 345kV bus.
90	FLT_090_P4THISCLARTHIS_THISTLE4_345_138kV_1PH	Loss of Clark County – Thistle 345kV CKT and Thistle 345/138/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Thistle 345kV bus.
91	FLT_091_P4THISWICHTHIS_THISTLE4_345_138kV_1PH	Loss of Thistle – Wichita 345kV CKT and Thistle 345/138/13.8kV transformer caused by a stuck breaker (16 cycle without reclose) attempting to clear a Single-Phase fault near the Thistle 345kV bus.
92	FLT_092_P6SPVLCLRKSPVL_IRONWOOD7_345kV_3PH	Prior outage of Clark County – Spearville 345kV CKT followed by system adjustments. Then 3-Phase fault on the Ironwood – Spearville 345kV CKT near the Spearville 345kV bus.
93	FLT_093_P7SPVLCLRKSPVL_IRONWOOD7_345kV_1PH	Single-Phase fault on the Ironwood – Spearville 345kV CKT and Clark County – Spearville 345kV CKT near the Spearville 345kV bus.
94	FLT_094_P6CLRKSPVLCLRK_IRONWOOD7_345kV_3PH	Prior outage of Clark County – Spearville 345kV CKT followed by system adjustments. Then 3-Phase fault on the Ironwood – Spearville 345kV CKT near the Clark County 345kV bus.
95	FLT_095_P7CLRKSPVLCLRK_IRONWOOD7_345kV_1PH	Single-Phase fault on the Ironwood – Spearville 345kV CKT and Clark County – Spearville 345kV CKT near the Clark County 345kV bus.

Contingency Number and Name		Description
96	FLT_096_P6DBLCLARKCOUNTY7_THISTLE7_345kV_3PH	<i>Prior outage of Clark County – Thistle 345kV CKT 1 followed by system adjustments. Then 3-Phase fault on the Clark County – Thistle 345kV CKT 2 near the Clark County 345kV bus.</i>
96_R1	FLT_096_P6DBLCLARKCOUNTY7_THISTLE7_345kV_3PH_R1	<i>Curtail 420MW of Generation near Spearville 345kV. Prior outage of Clark County – Thistle 345kV CKT 1 followed by system adjustments. Then 3-Phase fault on the Clark County – Thistle 345kV CKT 2 near the Clark County 345kV bus.</i>
97	FLT_097_P7DBLCLARKCOUNTY7_THISTLE7_345kV_1PH	<i>Single-Phase fault on the Clark County – Thistle 345kV CKT 1 and Clark County – Thistle 345kV CKT 2 near the Clark County 345kV bus.</i>
97_R1	FLT_097_P7DBLCLARKCOUNTY7_THISTLE7_345kV_1PH_R1	<i>Curtail 420MW of Generation near Spearville 345kV. Single-Phase fault on the Clark County – Thistle 345kV CKT 1 and Clark County – Thistle 345kV CKT 2 near the Clark County 345kV bus.</i>
98	FLT_098_P6DBLTHISTLE7_WWRDEHV7_345kV_3PH	<i>Prior outage of Thistle – Woodward 345kV CKT 1 followed by system adjustments. Then 3-Phase fault on the Thistle – Woodward 345kV CKT 2 near the Thistle 345kV bus.</i>
99	FLT_099_P7DBLTHISTLE7_WWRDEHV7_345kV_1PH	<i>Single-Phase fault on the Thistle – Woodward 345kV CKT 1 and Thistle – Woodward 345kV CKT 2 near the Thistle 345kV bus.</i>
100	FLT_100_P6DBLTHISTLE7_WICHITA7_345kV_3PH	<i>Prior outage of Thistle – Wichita 345kV CKT 1 followed by system adjustments. Then 3-Phase fault on the Thistle – Wichita 345kV CKT 2 near the Thistle 345kV bus.</i>
101	FLT_101_P7DBLTHISTLE7_WICHITA7_345kV_1PH	<i>Single-Phase fault on the Thistle – Wichita 345kV CKT 1 and Thistle – Wichita 345kV CKT 2 near the Thistle 345kV bus.</i>
102	FLT_102_P6DBLFTDODGE3_NFTDODG3_115kV_3PH	<i>Prior outage of Fort Dodge – North Fort Dodge 115kV CKT 1 followed by system adjustments. Then 3-Phase fault on the Fort Dodge – North Fort Dodge 115kV CKT 2 near the Fort Dodge 115kV bus.</i>
103	FLT_103_P7DBLFTDODGE3_NFTDODG3_115kV_1PH	<i>Single-Phase fault on the Fort Dodge – North Fort Dodge 115kV CKT 1 and Fort Dodge – North Fort Dodge 115kV CKT 2 near the Fort Dodge 115kV bus.</i>
104	FLT_104_P6NFTDSPVLNFTD_LANCER3_115kV_3PH	<i>Prior outage of North Fort Dodge – Spearville 115kV CKT 1 followed by system adjustments. Then 3-Phase fault on the Lancer – North Fort Dodge 115kV CKT 1 near the North Fort Dodge 115kV bus.</i>
105	FLT_105_P7NFTDSPVLNFTD_LANCER3_115kV_1PH	<i>Single-Phase fault on the North Fort Dodge – Spearville 115kV CKT 1 and Lancer – North Fort Dodge 115kV CKT 1 near the North Fort Dodge 115kV bus.</i>

## Power Factor Analysis and Reactor Requirements

Power factor analysis was performed for this study and is designed to demonstrate the reactive power requirements at the point of interconnection during the period of limited operation prior to the in service date of all required upgrades. Power factor analysis was performed both while the generator is dispatched at this study's determined limited output and off-line. In order to perform the analysis the request and equivalent transmission lines and collectors systems were modeled using specifications provided by the Customer.

*Table 9 - Power Factor Analysis and Reactor Requirements During LOIS Period*

Request	Capacity	POI	Fuel	Generator	Power Factor Requirements at POI	Reactor Requirements at POI for 0.0 MW
GEN-2011-016	200.1 MW	Spearville 345kV	Wind	Siemens 2.3MW	0.81pf lagging to 1.0pf	16.0 MVAR
GEN-2011-017	299.0 MW	Tap on Spearville to Post Rock 345kV	Wind	Siemens 2.3MW	0.81pf lagging to 0.977pf leading	14.0 MVAR

*NOTE: As reactive power is required for all projects, the final requirement in the GIA will be the pro-forma 95% lagging to 95% leading at the point of interconnection.*

Analysis shows that while generating at 200.1MW & 299.0 MW the voltages at the GEN-2011-016 POI & GEN-2011-017 POI are low for most system conditions requiring an injection of reactive power from GEN-2011-016 & GEN-2011-017 to the system. While the GIA will require the requests to maintain a 0.95pf lagging to 0.95pf leading at the POI, this analysis shows that during the limited operation period the voltage could be extremely deficient during high west to east transfers requiring some type of mitigation, increasing the chances of curtailment.

During periods where the requests are off-line or not generating, the approximate amount of charging current provided by the GEN-2011-016 subsystem is 17.7MVAR & GEN-2011-017 subsystem is 15.7 MVAR. To perform this analysis, the study projects generation was reduced to 0MW and 0MVAR with the collector systems remaining connected to the system. Should the configuration of the request collector systems change from what was submitted, a restudy of the reactor requirements may be required. All other non-dispatchable projects with adjacent POI's were disconnected from the system. It is recommended that the Customer install at least 17.7MVAR of reactors at GEN-2011-016 and 15.7MVAR of reactors at GEN-2011-017 to compensate for the injection of charging current into the transmission system. It is also recommended that all of this reactive support be installed at the POI to counter the injection of capacitance from the 345kV Customer substation lead. Should the Customer choose to not install all of the reactors at the POI, additional reactors may be required.

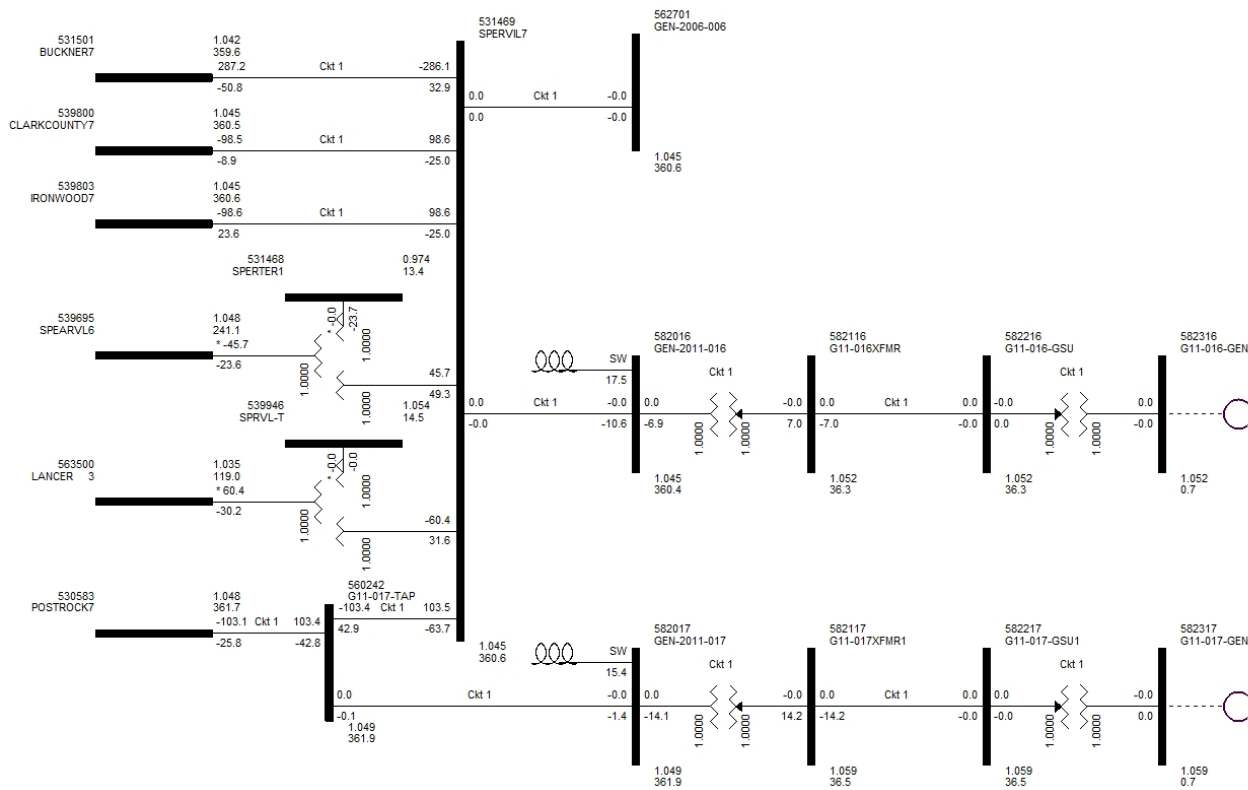


Figure 3: GEN-2011-016 & GEN-2011-017 with generators turned off and shunt reactors added to the high side of the substation 345/34.5kV transformers

## Results

Results of the stability analysis are summarized in Table 10. These results are valid for the Customers interconnecting with a generation amount up to 499.1 MW given the study assumptions. The results indicate that the transmission system remains stable for all single contingencies studied. A NERC Category “P7” event resulted in potential voltage instability. This instability can be mitigated with generation curtailments that limit the flows on the double circuit line from Clark County – Thistle 345kV. The plots will be available upon request.

Table 10: Fault Analysis Results for Limited Operation

Contingency Number and Name		2014WP	2015SP	2024SP
1	FLT_001_SPERVIL7_BUCKNER7_345kV_3PH	Stable	Stable	Stable
2	FLT_002_SPERVIL7_BUCKNER7_345kV_1PH	Stable	Stable	Stable
3	FLT_003_SPERVIL7_CLARKCOUNTY7_345kV_3PH	Stable	Stable	Stable
4	FLT_004_SPERVIL7_CLARKCOUNTY7_345kV_1PH	Stable	Stable	Stable
5	FLT_005_SPERVIL7_IRONWOOD7_345kV_3PH	Stable	Stable	Stable
6	FLT_006_SPERVIL7_IRONWOOD7_345kV_1PH	Stable	Stable	Stable
7	FLT_007_SPERVIL7_G11017TAP_345kV_3PH	Stable	Stable	Stable
8	FLT_008_SPERVIL7_G11017TAP_345kV_1PH	Stable	Stable	Stable
9	FLT_009_SPERVIL7_SPEARVL6_345_230kV_3PH	Stable	Stable	Stable
10	FLT_010_SPERVIL7_LANCER3_345_115kV_3PH	Stable	Stable	Stable
11	FLT_011_BUCKNER7_HOLCOMB7_345kV_3PH	Stable	Stable	Stable



Contingency Number and Name		2014WP	2015SP	2024SP
12	FLT_012_BUCKNER7_HOLCOMB7_345kv_1PH	Stable	Stable	Stable
13	FLT_013_HOLCOMB7_FINNEY7_345kv_3PH	Stable	Stable	Stable
14	FLT_014_HOLCOMB7_FINNEY7_345kv_1PH	Stable	Stable	Stable
15	FLT_015_HOLCOMB7_SETAB7_345kv_3PH	Stable	Stable	Stable
16	FLT_016_HOLCOMB7_SETAB7_345kv_1PH	Stable	Stable	Stable
17	FLT_017_HOLCOMB7_HOLCOMB3_345_115kv_3PH	Stable	Stable	Stable
18	FLT_018_FINNEY7_HITCHLAND7_345kv_3PH	Stable	Stable	Stable
19	FLT_019_FINNEY7_HITCHLAND7_345kv_1PH	Stable	Stable	Stable
20	FLT_020_IRONWOOD7_SPERVIL7_345kv_3PH	Stable	Stable	Stable
21	FLT_021_IRONWOOD7_SPERVIL7_345kv_1PH	Stable	Stable	Stable
22	FLT_022_IRONWOOD7_CLARKCOUNTY7_345kv_3PH	Stable	Stable	Stable
23	FLT_023_IRONWOOD7_CLARKCOUNTY7_345kv_1PH	Stable	Stable	Stable
24	FLT_024_CLARKCOUNTY7_THISTLE7_345kv_3PH	Stable	Stable	Stable
25	FLT_025_CLARKCOUNTY7_THISTLE7_345kv_1PH	Stable	Stable	Stable
26	FLT_026_THISTLE7_WICHITA7_345kv_3PH	Stable	Stable	Stable
27	FLT_027_THISTLE7_WICHITA7_345kv_1PH	Stable	Stable	Stable
28	FLT_028_THISTLE7_WWRDEHV7_345kv_3PH	Stable	Stable	Stable
29	FLT_029_THISTLE7_WWRDEHV7_345kv_1PH	Stable	Stable	Stable
30	FLT_030_THISTLE7_THISTLE4_345_138kv_3PH	Stable	Stable	Stable
31	FLT_031_WWRDEHV7_TATONGA7_345kv_3PH	Stable	Stable	Stable
32	FLT_032_WWRDEHV7_TATONGA7_345kv_1PH	Stable	Stable	Stable
33	FLT_033_WWRDEHV7_BORDER7_345kv_3PH	Stable	Stable	Stable
34	FLT_034_WWRDEHV7_BORDER7_345kv_1PH	Stable	Stable	Stable
35	FLT_035_WWRDEHV7_BEVERCO_345kv_3PH	Stable	Stable	Stable
36	FLT_036_WWRDEHV7_BEVERCO_345kv_1PH	Stable	Stable	Stable
37	FLT_037_WWRDEHV7_WWRDEHV4_345_138kv_3PH	Stable	Stable	Stable
38	FLT_038_BEVERCO_HITCHLAND7_345kv_3PH	Stable	Stable	Stable
39	FLT_039_BEVERCO_HITCHLAND7_345kv_1PH	Stable	Stable	Stable
40	FLT_040_WICHITA7_EMPEC7_345kv_3PH	Stable	Stable	Stable
41	FLT_041_WICHITA7_EMPEC7_345kv_1PH	Stable	Stable	Stable
42	FLT_042_WICHITA7_RENO7_345kv_3PH	Stable	Stable	Stable
43	FLT_043_WICHITA7_RENO7_345kv_1PH	Stable	Stable	Stable
44	FLT_044_WICHITA7_BENTON7_345kv_3PH	Stable	Stable	Stable
45	FLT_045_WICHITA7_BENTON7_345kv_1PH	Stable	Stable	Stable
46	FLT_046_WICHITA7_VIOLA7_345kv_3PH	Stable	Stable	Stable
47	FLT_047_WICHITA7_VIOLA7_345kv_1PH	Stable	Stable	Stable
48	FLT_048_G11017TAP_SPERVIL7_345kv_3PH	Stable	Stable	Stable
49	FLT_049_G11017TAP_SPERVIL7_345kv_1PH	Stable	Stable	Stable
50	FLT_050_G11017TAP_POSTROCK7_345kv_3PH	Stable	Stable	Stable
51	FLT_051_G11017TAP_POSTROCK7_345kv_1PH	Stable	Stable	Stable
52	FLT_052_POSTROCK7_AXTELL3_345kv_3PH	Stable	Stable	Stable
53	FLT_053_POSTROCK7_AXTELL3_345kv_1PH	Stable	Stable	Stable
54	FLT_054_POSTROCK7_POSTROCK6_345_230kv_3PH	Stable	Stable	Stable
55	FLT_055_AXTELL3_PAULINE3_345kv_3PH	Stable	Stable	Stable
56	FLT_056_AXTELL3_PAULINE3_345kv_1PH	Stable	Stable	Stable
57	FLT_057_AXTELL3_SWEETW3_345kv_3PH	Stable	Stable	Stable
58	FLT_058_AXTELL3_SWEETW3_345kv_1PH	Stable	Stable	Stable
59	FLT_059_AXTELL3_AXTELL7_345_115kv_3PH	Stable	Stable	Stable
60	FLT_060_SPEARVL6_GRTBEND6_230kv_3PH	Stable	Stable	Stable
61	FLT_061_SPEARVL6_GRTBEND6_230kv_1PH	Stable	Stable	Stable
62	FLT_062_SPEARVL6_SPEARVL3_230_115kv_3PH	Stable	Stable	Stable
63	FLT_063_GRTBEND6_CIRCLE6_230kv_3PH	Stable	Stable	Stable
64	FLT_064_GRTBEND6_CIRCLE6_230kv_1PH	Stable	Stable	Stable
65	FLT_065_GRTBEND6_HEIZER6_230kv_3PH	Stable	Stable	Stable
66	FLT_066_GRTBEND6_HEIZER6_230kv_1PH	Stable	Stable	Stable
67	FLT_067_SHAYS6_GRTBEND6_230kv_3PH	Stable	Stable	Stable
68	FLT_068_SHAYS6_GRTBEND6_230kv_1PH	Stable	Stable	Stable

Contingency Number and Name		2014WP	2015SP	2024SP
69	FLT_069_POSTROCK6_SHAYS6_230kV_3PH	Stable	Stable	Stable
70	FLT_070_POSTROCK6_SHAYS6_230kV_1PH	Stable	Stable	Stable
71	FLT_071_POSTROCK6_KNOLL6_230kV_3PH	Stable	Stable	Stable
72	FLT_072_POSTROCK6_KNOLL6_230kV_1PH	Stable	Stable	Stable
73	FLT_073_KNOLL6_SMOKYHL6_230kV_3PH	Stable	Stable	Stable
74	FLT_074_KNOLL6_SMOKYHL6_230kV_1PH	Stable	Stable	Stable
75	FLT_075_SMOKYHL6_SUMMIT6_230kV_3PH	Stable	Stable	Stable
76	FLT_076_SMOKYHL6_SUMMIT6_230kV_1PH	Stable	Stable	Stable
77	FLT_077_NFTDODG3_FTDODGE3_115kV_3PH	Stable	Stable	Stable
78	FLT_078_NFTDODG3_FTDODGE3_115kV_1PH	Stable	Stable	Stable
79	FLT_079_NFTDODG3_SSTATTP3_115kV_3PH	Stable	Stable	Stable
80	FLT_080_NFTDODG3_SSTATTP3_115kV_1PH	Stable	Stable	Stable
81	FLT_081_FTDODGE3_CRKCK3_115kV_3PH	Stable	Stable	Stable
82	FLT_082_FTDODGE3_CRKCK3_115kV_1PH	Stable	Stable	Stable
83	FLT_083_P4SPERBUCKSPER_SPEARVL6_345_230kV_1PH	Stable	Stable	Stable
84	FLT_084_P4SPERCLARSPER_SPEARVL6_345_230kV_1PH	Stable	Stable	Stable
85	FLT_085_P4SPERIRONSPER_SPEARVL6_345_230kV_1PH	Stable	Stable	Stable
86	FLT_086_P4SPER117SPER_SPEARVL6_345_230kV_1PH	Stable	Stable	Stable
87	FLT_087_P4AXTEPAULAXTE_AXTELL7_345_115kV_1PH	Stable	Stable	Stable
88	FLT_088_P4AXTESWEEAXTE_AXTELL7_345_115kV_1PH	Stable	Stable	Stable
89	FLT_089_P4THISWWRDTHIS_THISTLE4_345_138kV_1PH	Stable	Stable	Stable
90	FLT_090_P4THISCLARTHIS_THISTLE4_345_138kV_1PH	Stable	Stable	Stable
91	FLT_091_P4THISWICHTHIS_THISTLE4_345_138kV_1PH	Stable	Stable	Stable
92	FLT_092_P6SPVLCLRKSPVL_IRONWOOD7_345kV_3PH	Stable	Stable	Stable
93	FLT_093_P7SPVLCLRKSPVL_IRONWOOD7_345kV_1PH	Stable	Stable	Stable
94	FLT_094_P6CLRKSPVLCLRK_IRONWOOD7_345kV_3PH	Stable	Stable	Stable
95	FLT_095_P7CLRKSPVLCLRK_IRONWOOD7_345kV_1PH	Stable	Stable	Stable
96	FLT_096_P6DBLCLARKCOUNTY7_THISTLE7_345kV_3PH	Unstable	Unstable	Unstable
96_R1	FLT_096_P6DBLCLARKCOUNTY7_THISTLE7_345kV_3PH_R1	Stable	Stable	Stable
97	FLT_097_P7DBLCLARKCOUNTY7_THISTLE7_345kV_1PH	Unstable	Unstable	Unstable
97_R1	FLT_097_P7DBLCLARKCOUNTY7_THISTLE7_345kV_1PH_R1	Stable	Stable	Stable
98	FLT_098_P6DBLTHISTLE7_WWRDEHV7_345kV_3PH	Stable	Stable	Stable
99	FLT_099_P7DBLTHISTLE7_WWRDEHV7_345kV_1PH	Stable	Stable	Stable
100	FLT_100_P6DBLTHISTLE7_WICHITA7_345kV_3PH	Stable	Stable	Stable
101	FLT_101_P7DBLTHISTLE7_WICHITA7_345kV_1PH	Stable	Stable	Stable
102	FLT_102_P6DBLFTDODGE3_NFTDODG3_115kV_3PH	Stable	Stable	Stable
103	FLT_103_P7DBLFTDODGE3_NFTDODG3_115kV_1PH	Stable	Stable	Stable
104	FLT_104_P6NFTDSPVLNFTD_LANCER3_115kV_3PH	Stable	Stable	Stable
105	FLT_105_P7NFTDSPVLNFTD_LANCER3_115kV_1PH	Stable	Stable	Stable

### FERC LVRT Compliance

FERC Order #661A places specific requirements on wind farms through its Low Voltage Ride Through (LVRT) provisions. For Interconnection Agreements signed after December 31, 2006, wind farms shall stay on line for faults at the POI that draw the voltage down at the POI to 0.0 pu.

Fault contingencies were developed to verify that wind farms remain on line when the POI voltage is drawn down to 0.0 pu. These contingencies are shown in Table 11.

Table 11: LVRT Contingencies

Contingency Name	Description
FLT_001_SPERVIL7_BUCKNER7_345kV_3PH	3-Phase fault on the Buckner – Spearville 345kV CKT near the Spearville 345kV bus.

Contingency Name	Description
FLT_003_SPERVIL7_CLARKCOUNTY7_345kV_3PH	<i>3-Phase fault on the Clark County – Spearville 345kV CKT near the Spearville 345kV bus.</i>
FLT_005_SPERVIL7_IRONWOOD7_345kV_3PH	<i>3-Phase fault on the Ironwood – Spearville 345kV CKT near the Spearville 345kV bus.</i>
FLT_007_SPERVIL7_G11017TAP_345kV_3PH	<i>3-Phase fault on the GEN-2011-017-Tap – Spearville 345kV CKT near the Spearville 345kV bus.</i>
FLT_009_SPERVIL7_SPEARVL6_345_230kV_3PH	<i>3-Phase fault on the Spearville 345/230/13.8kV transformer near the Spearville 345kV bus.</i>
FLT_010_SPERVIL7_LANCER3_345_115kV_3PH	<i>3-Phase fault on the Spearville 345/115/13.8kV (Lancer) transformer near the Spearville 345kV bus.</i>
FLT_048_G11017TAP_SPERVIL7_345kV_3PH	<i>3-Phase fault on the GEN-2011-017-Tap – Spearville 345kV CKT near the GEN-2011-017-Tap 345kV bus.</i>
FLT_050_G11017TAP_POSTROCK7_345kV_3PH	<i>3-Phase fault on the GEN-2011-017-Tap – Post Rock 345kV CKT near the GEN-2011-017-Tap 345kV bus.</i>

The required prior queued project wind farms remained online for the fault contingencies described in this section as well as the fault contingencies described in the Disturbances section of this report. Customers are found to be in compliance with FERC Order #661A.

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## Conclusion

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<OMITTED TEXT> (Interconnection Customers GEN-2011-016 and GEN-2011-017) have requested a Limited Operation System Impact Study under the Southwest Power Pool Open Access Transmission Tariff (OATT) for a total of 499.1 MW of wind generation to be interconnected as an Energy Resource (ER) into the Transmission System of Sunflower Electric Power Corporation (SUNC) in Ford and Hodgeman County, Kansas. The point of interconnection for GEN-2011-016 will be the Spearville 345kV substation. The point of interconnection for GEN-2011-017 will be through a tap on Spearville – Post Rock 345kV transmission line. The Customers, under GIA Section 5.9, has requested this Limited Operation Interconnection Study (LOIS) to determine the impacts of interconnecting to the transmission system before all required Network Upgrades identified in the DISIS-2011-001 (or most recent iteration) Impact Study can be placed into service.

Power flow analysis from this LOIS has determined that the Customers request can interconnect their generation as an Energy Resource prior to the completion of the required Network Upgrades, listed within Table 2 of this report. Should any other projects, other than those listed within Table 1 of this report, come into service an additional study may be required to determine if any limited operation service is available. Refer to Table 4 and 5 for the Limited Operation Interconnection Service available due to interconnection constraints.

Transient stability analysis indicates that the transmission system will remain stable for the contingencies listed within Table 8 with the addition of the Customers generation. Additionally, the Customers were found to be in compliance with FERC Order #661A when studied as listed within this report.

Any changes to these assumptions, for example, one or more of the previously queued requests not included within this study execute an interconnection agreement and commencing commercial operation, may require a re-study of this LOIS at the expense of the Customer.

Nothing in this System Impact Study constitutes a request for transmission service or confers upon the Interconnection Customer any right to receive transmission service.